Stormwater Drainage Design

For

Temporary Shop and Services with Ancillary Office at Lot No. 1038A in D.D. 130

Fuk Hang Tsuen, Tuen Mun, N.T.

Report No.: LD/L1038A/DS01

Date: 16/7/2024

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Background

Due to the proposed development in Lot 1038A DD 130, surface runoff will be connected to the drainage system at the site by U-channels and catchpits. The runoff will be finally discharged to an existing drainage system. This report is to briefly assess the impact to the existing drainage system arising from the development.

Scope of Work

Determine the existing drainage condition & impact arising from the development and verify the adequacy of the downstream drainage to cater for the additional runoff in the proposed condition.

Assessment Cristeria and Methodology

- 1. Determine the catchment area of the existing drainage channel adjacent to Lot 1038A DD 130 to be affected.
- 2. Determine the runoff directions and land uses to assign suitable runoff coefficients to the catchments.
- 3. Determine the rainfall intensity for the catchments.
- 4. Determine the runoff by Rational Method as advised in the Stormwater Drainage Manual (SDM).
- 5. Determine the capacity of the affected channel.

1. Determine the Catchment for the Downstream Drainage

Refer to Appendix-A for the proposed catchment plan.

As shown, the catchment area of the development to be affected is 500 meter square.

2. Determine the Rainfall Intensity for the Catchment

2.1. Determine the Rainfall Intensity for the Catchment of the affected channel.

SDM

Catchment Area and Run-off (1 in 50-year)

Site Area, m²: 500

Proposed Application Site is concrete paved, C = 0.95

No Upstream Catchment

Prposed Development will be paved Area, C = 0.95

Catchment is small, so Rational Method is appropriate.

	Area, A	_f [1]	Intensity, i [2]	Runoff	noff Peak Runoff, Q _p ^[4]	
Catchment	Aica, A	Coefficient, C [3] Base Case Mid	Mid 21 st Century ^[5]			
	(m ²)	(min)	(mm/h)			(m^3/s)
Paved 100%	500	5	229	0.95	0.03	0.03

Remarks:

[1] The Application Site is flat. Time of concentration (t_d) is assumed to be 5 min.

[2] i = extreme mean intensity in mm/hr $(t_a + b)^c$ t_d = duration in minutes (t_d \leq 240)

a, b and c = storm constants

According to Table 3a - Storm Constants for Different Return Periods of HKO Headquarters of SDM:

Return Period	50 Years
a	451.3
ь	2.46
С	0.337

Value of C is made reference to Section 7.5.2 of DSD's SDM. [3]

 Q_p = peak runoff in m³/s $Q_p = 0.278C i A$ where [4] C = runoff coeficient (dimensionless)

i = rainfall intensity in mm/hr

 $A = \text{catchment area in km}^2$

The rainfall increse due to climate change for mid 21st century of 11.1% is adopted based on (k) of SDM -[5] Corrigendum No. 1/2022

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time of concentration (t_d) = natural flow time (t_0) + channel flow time (t_f)

SDM CI.7.5.2

$$t_0 = 0.14465 \frac{L}{H^{0.2} A^{0.1}}$$

For the affected channel section:

distance (L) = $\frac{25}{m}$

average slope (H) = (change in height)/L

$$H = (7.4 - 7.2) / 25$$

H = 0.80%

area of catchment(A)= 500 m^2

 $t_0 = 5.1 \quad \text{min}$

t_f=time of flow (which is assumed to be zero for conservative checking

 $t_f = 0 \quad min$

 $t_d = 5.1 \quad min$

SDM Cl. 4.3.2

$$i = \frac{a}{(t_d + b)^c}$$

where i is the rainfall intensity

Return period T (years) i =

2	5	10	20	50	100	200	500	1000
166	192	205	217	228	235	240	247	250

3. Determine Existing Flow to the affected channel

SDM Cl. 7.5.2

$$Q = 0.278i \sum_{j=1}^{m} CjAj$$

where m is the number of subcatchments refer to LD/L1038A/D01 for the existing catchment plan

mm/hr

Assumptions

SDM The whole catchment can be described by three types of catchment characteristics:

- 1. Grassland & paved.
- Cl. 7.5.2 2. Grassland catchment shall take a runoff coefficient of 0.35 as taken from the higher end of 0.35 "Steep Grassland" · C=0.25.
 - 3. Paved catchement shall take a runoff coefficient of 0.95 as taken from the higher end of "Concrete".
- 3.1. Summary of existing flow in the affected section of the channel in different return period

For the section of the channel to be affected

Return Period	Existing Flow (m ³ /s)
2	0.02
10	0.03
50	0.03
200	0.03

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4. Proposed Diversion for the affected section of channel

$$Q = A \frac{R^{1/6}}{n} \sqrt{RS} f$$

Use the Manning Equation to Determine the Drainage Capacity

Refer to Drawing No. LD/L1038A/D01, the alignment of proposed channel is indicated to suit for the proposed development. The proposed diversion comprise of 225mm concrete U-channel. The channel size and the capacity check are as follows.

Assumptions:

- 4.1 Roughless coefficient of proposed channel, n is 0.014 (Concrete-lined channels)
- 4.2 End of the proposed channel will connect with existing channel gradient would be a little bit flatter, say 1 in 150

Full-bore capacity of the proposed channel section

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Channel Width = 225 mm = 0.225 m

Channel Depth = 225 mm = 0.225 m

Hydraulic Gradient, S_f = 0.0067

Gradient 1 in = 150

A = 0.0506 m^2

P = 0.675 m

R = 0.075 m

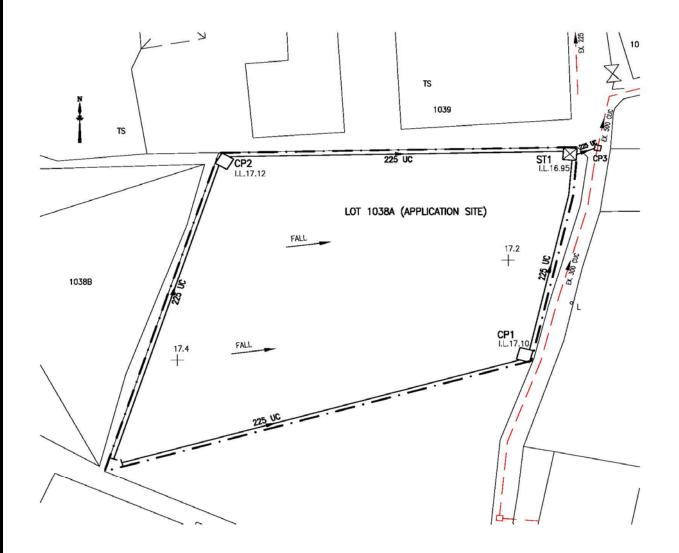
Full bore capacity = 0.0525 m^3/s
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The capacity of the proposed channel is larger than the highest capacity of Return Period 1 in 200 (0.03 m^3/s). Therefore, used 225mm UC is adequate for catchment Area of A.

5. CONCLUSION

- 5.1 A Drainage Impact Assessment has been conducted to evaluate the potential drainage impact due to the proposed drainage system.
- 5.2 The Drainage Impact Assessment has demonstrated that subject to the implementation of the proposed drainage system would not cause adverse drainage impact or an increase in the flooding susceptibility of the adjacent areas.
- 5.3 It is concluded that the Proposed Development will not result in any adverse drainage impact to the existing drainage system.

Appendix - A



Plan of Catchment Areas NTS

PLANS

LD/L1038A/FIG1 Location of Application Site

LD/L1038A/D01(A) Proposed Drainage Layout Plan

